中国科学院武汉岩土力学研究所

Mechanical Stability Assessment of China's Sedimentary Basins for Industrial-Scale CO₂ Geological Storage 考虑场地力学稳定性的储存场地选址方法

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Outline of Talk

汇报提纲

- 1. Project root
- 2. Research Background
- 3. Methodology
- 4. Technical accomplishment
- 5. Results and Products
- 6. Acknowledgements







2. Research Background of Geomechanics

2.1 Geomechanical Baseline Associated with CO₂ Injection





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COMPONENT

4.4.5 Baseline geomechanical characterization

Geomechanical characterization of a least the storage unit and the primary sear (saprock) shall be conducted based on well logs, in situ testing, or laboratory testing on preserved core material where possible, other overlying units should be characterized). Geomechanical characterization shall include the following:

- (a) evaluation of the natural seismicity and tectonic activity of the region where the prospective storage unit is to be located. In some cases, natural seismicity and tectonic activity can cause fracturing or fault reactivation, processes that can create or enhance permeable leakage flow paths. Accordingly, the available information related to seismicity and tectonic activities shall be collected and analyzed;
- (b) characterization of the in situ stress regime (magnitude and orientation of principal stresses). Wireline logs (especially density, sonic, and oriented caliper and borehole imager logs), small-scale hydrauli fracture tests (i.e., micro-fracture or mini-fracture tests), and leak-off tests can provide this information and should be performed prior to injection of the CO₂ stream. In the case of mature oil fields, the reservoir pressure at the time these measurements are made should also be recorded, given that pressure change generally induces changes in stress magnitudes. This information, used with the geomechanical modelling procedures described in Clause 4.5.5 can be used to assess injection pressure limits. Similarly, although the minimum in situ stress in the storage unit (often referred to as the fracture pressure) may be used to define injection pressure limits in some cases, given that tensile fracturing or natural fracture reopening can occur once the injection pressure exceeds this stress magnitude, pressure limits should be assessed on the basis of a broader range of possible fracturing modes, as described in Clause 4.5.5;
- (c) determination of rock mechanical properties, which include (i) strength and deformation properties (e.g., Poisson's ratio and Young's modulus); (iii) thermal properties (e.g., thermal expansion coefficient, specific heat capacity, and thermal conductivity); and (iii) the attributes (e.g., orientation,

从本底调查阶段 到场地关闭后, 都必须进行详细 的力学评价!

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GUIDELINES FOR INITIAL CHARACTERIZATION

Guidelines for Initial Characterization.



2. Research Background of Geomechanics

2.4 Question



3. Methodology

3.1 Prerequisite

Killer criteria:

1. Potential theoretical capacity of basin (less than 2500 Mt)

2. Maximum thickness of potential storage basin greater than 1500 m)

3. Temperature of storage aquifer (less than 373 K)

4. Active fault to the injection well (R_f no less than 10 km)

必要条件:

- 1) 盆地理论容量小于2500 Mt
- 2) 沉积盆地厚度大于1500 m
- 3)储层温度高于373 K
- 4)活断层到注入井最短距离**R**,小于10 km

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3. Methodology

3.2 Prerequisite





3. Methodology

3.3 Logical flow of assessment



3. Methodology

3.4 Database Sources





4. Technical accomplishment

Index→Flow→Mapping





5. Results and Products

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5.1 Resultant Mapping



6. Results and Verification



Computation models and numerical analyses: Verification

1	M_{θ} Source: Mathias et al. 2009	$P \rightarrow P \left[1_{1e} \left(t_e \right) \right] + 1$	$1 \left[\frac{\alpha}{1 - \varepsilon} \left(\alpha \right) + \varepsilon \right] + \rho \right]$	参数	取值
+	↓ · · · · · · · · · · · · · · · · · · ·	$P_t \approx P_e \left\{ -\frac{1}{2} \ln \left(\frac{1}{2\gamma t} \right)^{-1} + \frac{1}{\gamma} - \frac{1}{2\gamma} \right\}$ If	$\frac{1}{2\gamma} \prod_{j=1}^{m} \left(\frac{1}{2\gamma^2} \right)^{+\zeta} + \zeta^{-1} $	杨氏模量, [Pa]	3.0x10 ⁹
	CO2 H h(r, t) Brine r 注入井 注覆地层 W	$P_{e} = \frac{M_{0}\mu_{0}}{2\pi H\rho_{0}k}$ $t_{e} = \frac{2\pi\phi Hr_{w}^{2}\rho}{M_{0}}$ $\gamma = \frac{\mu_{0}}{\mu_{w}}$	$M_0\mu_0$	波松比,[-]	0.25
			$P_{e} = \frac{0.0}{2\pi H \rho_{e} k}$	岩石密度, [kg/m³]	2800
. .			_ ~11 p ₀ ~	流体密度, [kg/m ³]	980
			$2\pi\phi Hr_w^2\rho_0$	初始孔隙度, [-]	0.23
			$t_e = \frac{M_e}{M_e}$	比奥系数, [-]	0.28
				比奥模量, [Pa]	1.3x10 ¹⁰
r			$_{\nu}$ – μ_0	孔隙压缩性, [1/Pa]	1.0x10-9
4			$\gamma - \frac{1}{\mu_w}$	摩擦角,[º]	28
I				粘聚力, [Pa]	2.0x10 ⁷
		$\alpha = \frac{M_0 \mu_0 (c_r + c_w)}{2\pi H \rho_0 k}$ $\beta = \frac{M_0 k b}{2\pi H r_w \mu_0}$	$\alpha = \frac{M_0 \mu_0 (c_r + c_w)}{M_0 (c_r + c_w)}$	初始渗透率, [m ²]	5.0x10 ⁻¹³
-			$2\pi H \rho_0 k$	注入压力, [Pa]	5.0x10 ⁷
L.			1644	粘性系数, [Pa-s]	1.3x10-3
			$\beta = \frac{M_0 \kappa \rho}{1 - 1 - 1}$	注入温度, [K]	293
深			流体热容, [J/kg/K]	1160	
度				固体热容, [J/kg/K]	920
[米]	二氧化	碳+咸水		流体热扩展系数, [1/K]	5.0x10-4
伯		咸水		固体热扩展系数, [1/K]	1.0x10-5
	۱ ۱۱٬ ۲۰٬ ۱۱٬			热导系数, [W/m/K]	2.63
				热扩散系数, [m²/s/K]	6.0x10 ⁻¹²
古	表岩			注入浓度, [mol/m3]	628
	离注入井的距离	[[米]	7	有效溶质扩散系数, [m²/s]	50x10-9
				地球化学反应率, [1/s]	1.0x10-9
	China Aus	stralia Geological Stora	ge of CO ₂	地球化学反应热, [J/mol]	
U		一与小理业日	白井左		
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6. Results and Verification

Future work



6. Acknowledgements

致谢



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CAS中国科学院MOST ACCA21科技部21世纪议程管理中心AIST Japan日本地质调查所Geoscience Australia澳大利亚地球科学局AITF Canada加拿大阿尔伯塔研究理事会CHEG CGS中国地调局水环中心

Thank you!

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